

TRANSPORTATION PROJECT REPORT

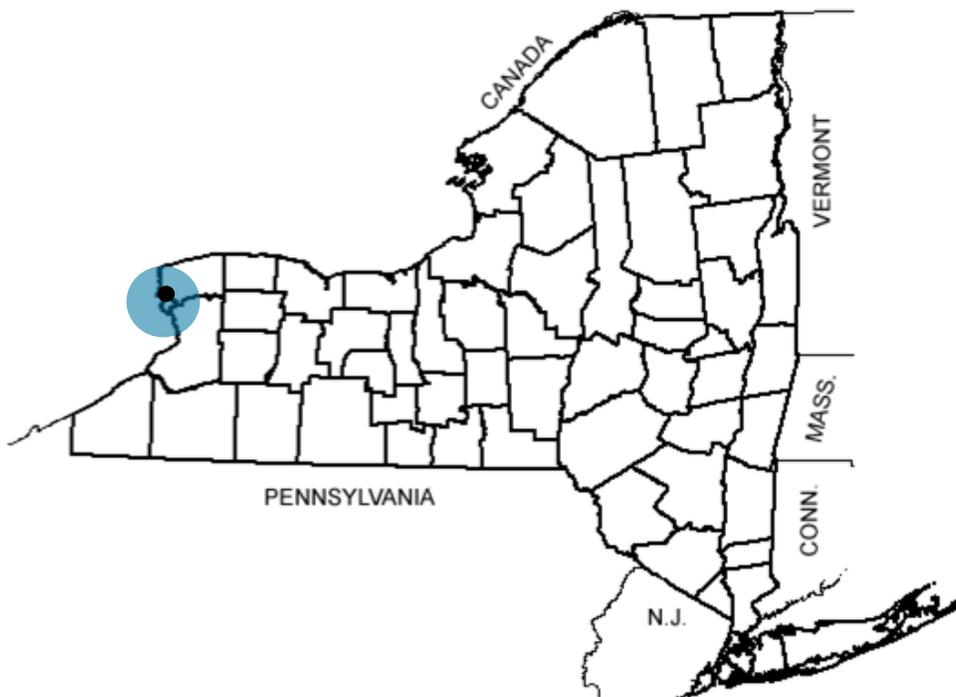
DRAFT DESIGN REPORT / DRAFT ENVIRONMENTAL IMPACT STATEMENT / DRAFT 4(f) EVALUATION

APPENDIX B5

Stormwater

November 2016

PIN 5470.22
NYS Route 198 (Scajaquada Expressway Corridor)
Grant Street Interchange to Parkside Avenue Intersection
City of Buffalo
Erie County



ANDREW M. CUOMO
Governor

Department of
Transportation

MATTHEW J. DRISCOLL
Commissioner



U.S. Department of Transportation
Federal Highway Administration

**APPENDIX B5
Stormwater**

TABLE OF CONTENTS

| | <u>Page Number</u> |
|---|--------------------|
| COVER | |
| TABLE OF CONTENTS | |
| B5.1. Introduction..... | 1 |
| B5.2 Alternative Description..... | 1 |
| B5.3. Watershed Area..... | 1 |
| B5.4. SPDES General Permit Requirements and Concepts..... | 1 |
| B5.5. Lane Miles of Roadway and Impervious Area Review..... | 4 |
| B5.6. Effects of De-Icing Chemicals..... | 4 |
| B5.7. Highway Runoff And Pollutant Loading Analysis..... | 5 |
| B5.8. References..... | 6 |

TABLES

| | |
|--------|--|
| B5.4-1 | Summary of Water Quality Volumes by Stage (Page 3) |
| B5.5-1 | Summary of Roadway Lane Miles and Impervious Area (Page 4) |
| B5.6-1 | Summary of Toler Method Chloride Concentrations (Page 5) |
| B5.7-1 | Annual Pollutant Loading Summary (Page 6) |

EXHIBITS

| | |
|-----------|--|
| Exhibit A | Existing and Redeveloped Impervious Areas Figure |
| Exhibit B | Water Quality Storm Water Management Locations |
| Exhibit C | Effluent Limitation Guidelines |
| Exhibit D | Water Quality Volume Preliminary Sizing Computations |
| Exhibit E | Toler Method Calculations |
| Exhibit F | Pollutant Loading Calculations |

B5.1. Introduction

NYS Route 198 (the Scajaquada Expressway) within the project area is an Urban Principal Arterial Expressway on the National Highway System connecting Grant Street and Parkside Avenue with traffic volumes between 38,000 and 50,000 vehicles per day, a posted speed limit of 30 mph, and grade separated interchanges. While providing an important transportation function, the Scajaquada Expressway is out of context with much of its surroundings, which includes a nationally renowned art gallery, educational institutions, a historic cemetery, historic buildings, residential neighborhoods, the aesthetic and historic Olmsted-designed Delaware Park, and Scajaquada Creek.

The purpose of this action is to address transportation deficiencies, including:

- Geometric features that do not meet current expressway standards
- Traffic congestion that occurs at one or more locations during peak periods
- Disparity between vehicular operating speeds, the posted speed limit, and design speed
- Higher than expected accident rates, accident severity, and identifiable accident patterns
- Deteriorating drainage systems that no longer function as designed and release untreated storm water into Scajaquada Creek

Furthermore, this action is also to convert the Scajaquada Expressway into a feasible and prudent Urban Principal Arterial (non-expressway) transportation facility that operates in a safe manner and in greater harmony with the surrounding community character and natural environment. This involves providing improved visual and functional connectivity between the various features and resources throughout the adjacent area.

B5.2. Alternative Description

The Build Alternative addresses the needs of the Scajaquada corridor by transforming NYS Route 198 from an urban expressway into an urban boulevard with two travel lanes in each direction between Grant Street and Parkside Avenue, in its current location. Ramps at Grant Street, Elmwood Avenue, and Delaware Avenue would be replaced with connecting roadways. Roundabouts or signalized intersections would be constructed where each connecting roadway meets NYS Route 198. Parkside Avenue would remain a signalized intersection because a roundabout would not have adequate capacity to handle the expected volume of traffic, resulting in congestion and backups along both NYS Route 198 and Parkside Avenue. Transition zones would be developed using appropriate geometric and traffic calming features just west of Grant Street and just east of Parkside Avenue to encourage lower speeds and to signify entry to the corridor.

B5.3. Watershed Area

The watershed area identified within the project area is Scajaquada Creek, which also contains sub-watershed areas for the adjacent Mirror and Hoyt Lakes. It is noted that Scajaquada Creek and Hoyt Lake ("Delaware Park Lake") are listed on the Final New York State 2014 Section 303(d) List of Impaired Waters Requiring a TMDL. For the Build Alternative, approximately 34.2 acres (138,461 square meters) of post-construction disturbed impervious area would drain into Scajaquada Creek, Mirror Lake, and Hoyt Lake. The post-construction impervious area would be a reduction of 5.3% of the existing 36.1 acres (square meters) of impervious area. The preliminary values assume all roadways, sidewalks, and shared-use pathways as impervious surfaces.

B5.4. SPDES General Permit Requirements and Concepts

Site disturbance for the Build Alternative is calculated to be greater than 1 acre (0.4 hectare), therefore, a Stormwater Pollution Prevention Plan (SWPPP) would be required for compliance with the New York State Department of Environmental Conservation (NYSDEC) State Pollutant Discharge Elimination System (SPDES) General Permit for Stormwater Discharges from Construction Activity (Permit No. GP-0-15-002).

The project SWPPP document would include the following requirements: Erosion and Sediment Control (E&SC) Plans; description of the reduction in stream channel erosion, application of runoff reduction via green infrastructure techniques, prevention of overbank flooding and control of extreme flood events (water quantity controls), and stormwater management practices to provide for pollutant removal (water quality controls).

For the Build Alternative, E&SC measures would potentially include silt fence, drainage structure inlet protection, pipe inlet/outlet protection – pipe slope drain, stone check dams, stabilized construction entrances, seeding/soil stabilization operations and other practices as appropriate.

As this project involves disturbance and reconstruction of existing impervious surfaces, including realigning, replacing and removal of existing roadways with an overall reduction of impervious area, the entire project is being treated as redevelopment activities. Water quantity controls (Channel Protection Volume (Cpv), Overbank Flood (Qp), and Extreme Storm (Qf)) for the project that discharges into Scajaquada Creek, Mirror Lake, and Hoyt Lake would be waived. Redevelopment criteria in Chapter 9 of the NYS Stormwater Design Manual (SMDM 2015) state in Section 9.2.1 “Sizing Criteria” that if redevelopment activities result in no change to hydrology that increases the discharge rate from the project site, the 10-year and 100-year criteria do not apply. Discharge rates of stormwater runoff into Scajaquada Creek, Mirror Lake, and Hoyt Lake will not be increased because there is a proposed reduction in impervious cover within the project area.

For water quality control, the water quality volume (WQv) calculation assumes a disturbed area of approximately 65 acres (262,208 square meters). The actual disturbed area will be refined as the project details are developed during final design.

$$WQv = \frac{[(P)(Rv)(A)]}{12}$$

Where:
 WQv = water quality volume in (acre-feet)
 P = 90% rainfall event number (inches)
 Rv = 0.05+0.009(I), where I % impervious cover
 A = contributing area (acres)

It is assumed that the project will be constructed in two stages. It is typically required that for each stage of construction, stormwater management features be constructed in that stage, or possibly a prior stage that meets the requirements for that stage. The current proposed construction sequence includes: Contract 1 (Elmwood Avenue Section and Delaware Avenue to Parkside Avenue Section); and Contract 2 (Grant Street Section).

Required WQv's were calculated for each stage based on the amount of impervious surface and disturbed area in each stage. Both Contracts 1 and 2 have net impervious surface reduction. Exhibit A depicts the existing and redeveloped impervious areas. Within Contract 1, due to the constraints of the project, including lack of right-of-way, adjacent parkland, topography, etc., the WQv will be treated solely by non-standard underground hydrodynamic separators, a proprietary alternative device approved by NYSDEC as a method of water quality treatment. As such, the required treatment volume by alternative practices for Contract 1 is computed using the following calculation:

$$\%WQv \text{ Treatment by Alternative Practices} = \{25 - (\% \text{Impervious Cover Reduction} - \% \text{ WQV treated by Standard Practices} - \% \text{ Runoff Reduction})\} * 3$$

Contract 1 (Elmwood Avenue and Delaware Avenue to Parkside Avenue Sections) %WQv Treatment by Alternative Practices = {25 – (4 – 0 – 0)} x 3 = 63% of the WQv for redevelopment activities.

Contract 2 (Grant Street Section) will be treated by standard practice treatments, and thus is only required to provide 25% of the WQv for redevelopment activities.

Several potential water quality treatment areas have been identified within the project area to meet the water quality treatment volume requirements of the proposed activities. At this time, treatment areas have been identified to provide the necessary treatment within each stage. The proposed water quality treatments include wet swales, bioretention areas and hydrodynamic separators spread throughout the project corridor. Exhibit B depicts the approximate location of the potential water quality management areas.

The following table gives an approximate break up of water quality requirements and facilities provided assuming a three stage construction. Detailed calculations are located in Exhibit D.

| Table B5.4-1 Summary of Water Quality Volumes by Stage | | |
|---|--|-------------------------------------|
| Stage | Contract 1 | Contract 2 |
| Approximate Limits | Elmwood Avenue and Delaware Avenue to Parkside Avenue Sections | Grant Street Section |
| Water Quality Volume Required | 1.375 ac-ft (1,696 m ³) | 0.164 ac-ft (202 m ³) |
| Number of Facilities Provided | 9 | 4 |
| Facility Types | Hydrodynamic Separators | Bioretention Wet Swales |
| Water Quality Volume Provided | 1.686 ac-ft (2,080m ³) | 0.342 ac-ft (422 m ³) |
| Net Water Quality Volume | +0.311 ac-ft (+384 m ³) | +0.178 ac-ft (+220 m ³) |

The proposed hydrodynamic separators within Contract 1 will be designed to treat roadway runoff within the corridor and be placed beneath the roadway or adjacent to the roadway minimizing the need for additional right-of-way and impacts to the adjacent Delaware Park. The exact configuration of the devices will be determined during final design. The relatively high bedrock conditions in the project corridor (which is known to range between 7 and 14 feet below grade) is of concern for underground treatment. Borings and rock cores will be conducted during final design to ensure that the proposed locations of the underground facilities will be constructible. The effects associated with potential adjustments to the hydrodynamic separators will be determined during final design.

Additionally, all of the proposed shared-use paths throughout the corridor are currently assumed to be impervious surfaces. Conversion of portions of the shared-use paths to pervious surfaces including pervious pavement will be determined during final design. The conversion of these areas to pervious surfaces will further reduce the amount of stormwater treatment required.

Options for treating portions of impervious surfaces on the Buffalo State campus within the project corridor would be further investigated during final design. If reasonable, additional water quality treatment would be added to the western construction stage.

The project construction staging and sequencing has not yet been finalized, and as a result, the amount of disturbed area open at one time during construction has not been established. The E&SC Plan would include appropriate measures to address the final design. The NYSDEC has set regulations for Effluent Limitations for all projects covered under SPDES Permit No. GP-0-15-002 in New York State. These requirements are provided in Exhibit C.

B5.5. Lane-Miles of Roadway and Impervious Area Review

Post-construction activities of the Build Alternative would decrease the number of lane-miles (lane-kilometers) of roadways as well as decrease the amount of impervious surfaces in the project area (lane-miles are defined as the measure of the total length of traveled pavement surface, where lane-miles is the centerline length (in miles) multiplied by the number of lanes). Please note that even though there would be a reduction in lane-miles for the Build Alternative, the number of travel lanes would be the same as the No-Build Alternative and existing conditions. Lane-miles and impervious area are variables used in subsequent sections to determine water quality impacts in comparison to the No-Build Alternative. A detailed analysis during final design would determine ground disturbance values and other highway related factors. The No-Build and Build number of lane-miles and impervious roadway surface area values were calculated using project design files in Microstation CADD. Table B5.5-1 provides a summary of the roadway lane-miles and impervious area for Build Alternative.

| Table B5.5-1 Summary of Roadway Lane Miles and Impervious Area | | |
|---|--|--|
| | Lane- Miles (Lane-Kilometers) | Net Impervious Area, ac (m²) |
| No-Build Alternative | 16.2 (26.1) | 36.1 (146,090) |
| Build Alternative | 15.9 (25.6) | 30.2 (122,215) |
| Percent Difference | -1.9% | -16% |

B5.6. Effects of De-Icing Chemicals

Sodium and calcium chloride salts are used to maintain safe travel conditions during winter months. These de-icing salts reach surface water in the form of highway runoff and can affect the overall water quality of the Scajaquada Creek and Hoyt Lake drainage basins. The Toler Method is a predictive methodology that can be used to determine potential chloride concentrations in surface water from existing and anticipated salt applications on adjacent roadways (Toler, 1973). It was assumed that all the applied salt is diluted by the runoff generated, and all salt enters the two waterbodies under consideration, the Scajaquada Creek and Hoyt Lake. The method requires, as input, the following variables:

- T= Tons of salt per lane-mile, applied, per year
- M= Number of lane miles
- P= Annual Precipitation = 36.7 inches
- I= Inches of surface runoff, per year = (runoff coefficient) x P
- A= Drainage area, in square miles
- K= Conversion factor to yield Chloride concentration in mg/L = 8.37

The deicing compounds and their application rates are dependent upon the practices of agencies responsible for operations of the various roadways in the project area. Published NYSDOT application information shows approximately 0.81 tons per lane mile per snow event. The NYSDOT applies rock salt to NYS Route 198 at a rate of 27 tons per lane-mile per year (Schick, June 2005); this value was used for NYS Route 198 and all associated access ramps and roadways. The average application rate for roadways is 10 tons per lane-mile per year (Toler 1975); this rate was used for all other local roads that anticipate construction within the project area.

The pavement surfaces from the project area, which extends from approximately 2,600 feet (790 meters) east of Interstate 190 to Main Street, discharge into both the Scajaquada Creek and Hoyt Lake. The drainage area to Hoyt Lake is approximately 25.8 square miles, approximately 0.11 square miles of which comes from the project site. The drainage area to Scajaquada Creek at the end of the project area is approximately 26.7 square miles, of which approximately 0.08 square miles comes from the project site. Calculations applying the Toler Method were performed for the Build Alternative and compared to the calculated No-Build Alternative, neglecting the base contribution from the remainder of the watershed. The values are only for comparison purposes and do not accurately reflect the full concentration of chloride entering the waterbodies. Results indicate that the annual average chloride concentrations in runoff from the total project area would be 8.1 mg/L for the No-Build Alternative and 7.8 mg/L for Build Alternative.

The Toler Method was also used to analyze runoff within the Hoyt Lake watershed, which receives runoff from the eastern end of the project corridor. Even though overall there are less lane-miles under the Build Alternative compared to the No-Build Alternative, the portion of the highway that drains to Hoyt Lake has 0.2 lane-miles under the Build Alternative; therefore, the annual average chloride concentrations of runoff to Hoyt Lake would be slightly higher under the Build Alternative (4.4 mg/L for the No-Build Alternative and 4.6 mg/L for the Build Alternative). Detailed calculations are provided in Exhibit E, and the summary results are presented in Table B5.6-1.

| Site Condition | Average Annual Chloride Concentrations Scajaquada Creek – Entire Project Area (mg/L) | Average Annual Chloride Concentrations Sub Area Draining to Hoyt Lake (mg/L) |
|-----------------------|---|---|
| No-Build Alternative | 8.1 | 4.4 |
| Build Alternative | 7.8 | 4.6 |
| Percent Difference | -3.7% | 4.5% |

B5.7. Highway Runoff and Pollutant Loading Analysis

Urban highway runoff includes many vehicular by-products. Including metals, oil and grease, and soluble compounds formed by the combination of precipitation and vehicle exhausts. Potential water quality impacts may result from overland runoff that includes sedimentation, increased water temperatures and increased toxic substances, such as heavy metals, pesticides, oil and synthetic organic compounds. Many of these effects directly correspond to the amount of impervious paved road areas nearby. The "Simple Method" was utilized in providing gross analysis results of the No-Build Alternative and the Build Alternative (see Table B5.7-1 below). Detailed calculations are provided in Exhibit F. The pavement removal proposed for the Build Alternative would result in a 16% reduction of the pollutants analyzed for this project (not including shared-use paths within the impervious area calculations). The additional water quality treatment provided would further reduce the pollutant loadings associated with Build Alternative. This analysis demonstrates the pollutant loading differences between the No-Build Alternative and the Build Alternative, evaluated only with regard to the impervious areas within the project area, not including potential shared-use paths. The summary is provided as a method of comparison of the No-Build Alternative and the reduction of each known pollutant, assuming that the remainder of the watershed remains unchanged.

| Table B5.7-1 Annual Pollutant Loading⁽¹⁾ Summary | | | | |
|--|-----------------------------|---------------------------|--|---|
| Pollutant | No-Build Alternative | Build Alternative | Total Pollutants Removed By WQv Treatment | Total Reduction Of Build From No Build Alternative |
| Total Suspended Solids (TSS) | 37,244 lbs (16,894 kg) | 31,106 lbs (14,109 kg) | 18,121 lbs (8,219 kg) | 65% |
| Total Phosphorus (TP) | 84 lbs (38 kg) | 70 lbs (32 kg) | 43 lbs (19.5 kg) | 68% |
| Total Nitrogen (TN) | 787 lbs (357 kg) | 657 lbs (298 kg) | 138 lbs (62.6 kg) | 34% |
| Copper (Cu) | 14 lbs (6 kg) | 12 lbs (5 kg) | 2.3 lbs (1.0 kg) | 32% |
| Lead (Pb) | 105 lbs (48 kg) | 88 lbs (40 kg) | -- | 16% |
| Zinc (Zn) | 86 lbs (39 kg) | 72 lbs (33 kg) | 14 lb (6.3 kg) | 33% |

⁽¹⁾Pollutant Concentrations are obtained from Table 2.1 "Natural Median Concentrations for Chemical Constituents in Stormwater," Chapter 2 of the New York State Stormwater Management Design Manual, 2015

Common impacts associated with road construction and maintenance include habitat disruption, hydrologic alterations, and pollutant runoff. Runoff from road construction can cause erosion, sedimentation, and other changes disrupting aquatic habitats such as fish spawning areas and river bottom sediments (USEPA, 1996). The preservation of existing natural vegetative buffer strips along stream corridors is one way of reducing the impacts of highway runoff on receiving waterbodies and helping to maintain pre-development surface water quality.

B5.8. References

Center for Watershed Protection 2015. New York State Stormwater Design Manual. New York State Department of Environmental Conservation.

Toler, L. 1973. Effect of De-Icing Chemicals on Surface and Ground Water (Preliminary Guidelines for Estimating Chlorides). Research Project R-18-0 Interim Report.

USEPA. 1996. Indicators of the Environmental Impacts of Transportation- Highway, Rail, Aviation and Maritime Transport. EPA 230-R-96-009.

National Pollutant Removal Performance Database, Version 3. September 2007. Center for Watershed Protection

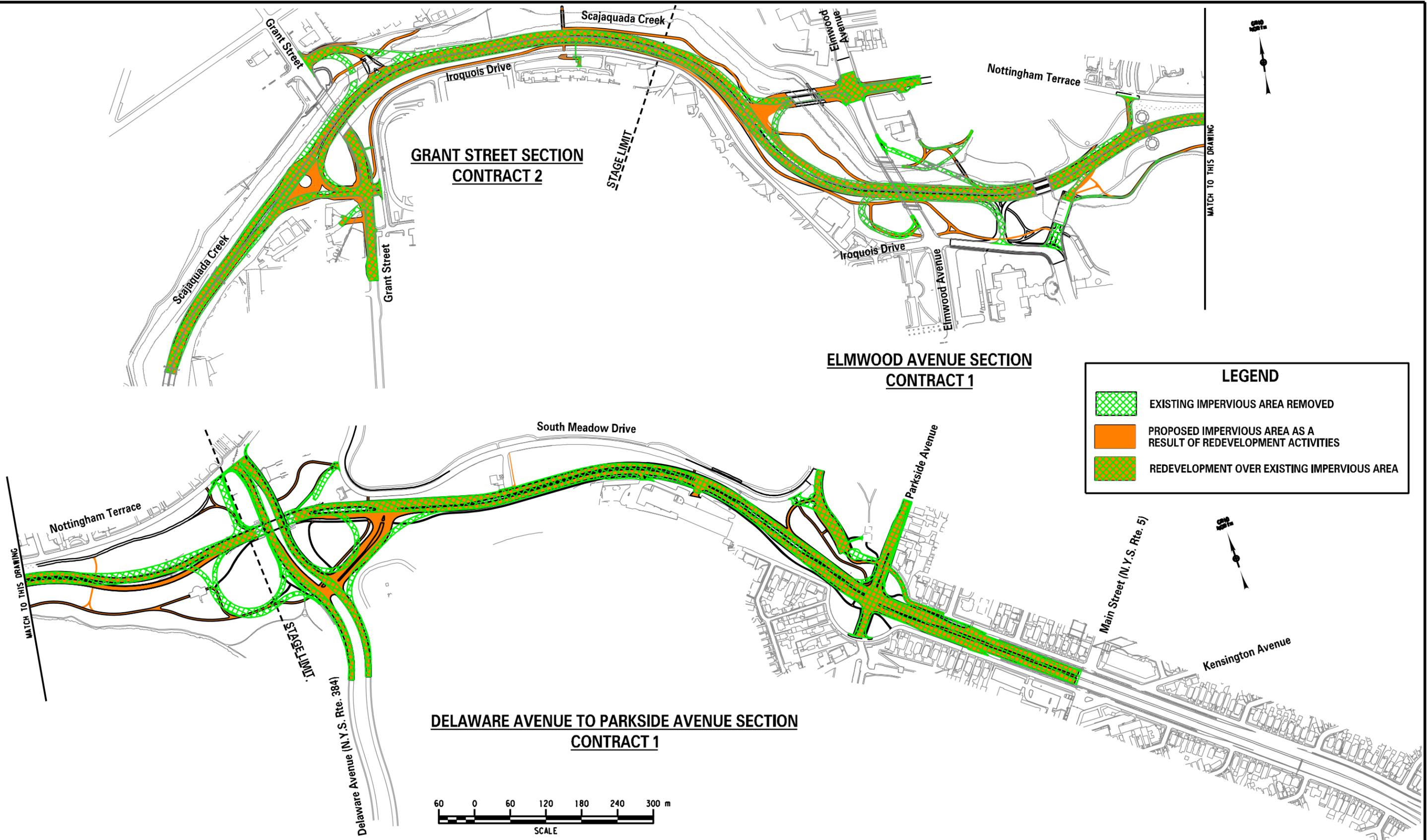
New Hampshire Stormwater Manual, Volume 2. December 2008. New Hampshire Department of Environmental Services.

EXHIBIT A

EXISTING AND REDEVELOPED IMPERVIOUS AREAS FIGURE

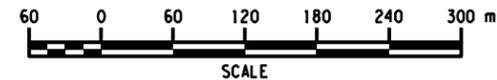
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LEGEND

- EXISTING IMPERVIOUS AREA REMOVED
- PROPOSED IMPERVIOUS AREA AS A RESULT OF REDEVELOPMENT ACTIVITIES
- REDEVELOPMENT OVER EXISTING IMPERVIOUS AREA



| | | | | | | |
|---|---|--------------|---------|----------|--|---|
| AS-BUILT REVISIONS DESCRIPTION OF ALTERATIONS: | N.Y.S. ROUTE 198 (SCAJAQUADA EXPRESSWAY CORRIDOR) | PIN 5470.22 | BRIDGES | CULVERTS | ALL DIMENSIONS IN m UNLESS OTHERWISE NOTED | CONTRACT NUMBER D031048-04 |
| | CITY OF BUFFALO | OCTOBER 2016 | | | | EXISTING AND REDEVELOPED IMPERVIOUS AREAS ALTERNATIVE 2 |
| | COUNTY: ERIE | | | | | |

IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR, TO ALTER AN ITEM IN ANY WAY, IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION.

EXHIBIT B

WATER QUALITY STORMWATER MANAGEMENT LOCATIONS

IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR, TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION.

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 DATE/TIME = DGN\$USER\$NAME
 USER = DGN\$USER\$NAME

DESIGN SUPERVISOR _____ JOB MANAGER _____ DESIGNED BY _____ ESTIMATED BY _____ DRAFTED BY _____ CHECKED BY _____



| | |
|----------------------------|--------------------|
| PREPARED BY: ON: | ALTERED BY: ON: |
| SIGNATURE _____ DATE _____ | |
| DOCUMENT NAME: | |

| | | | | | | | |
|--|--|-----------------------------|---------|----------|--|-----------------|---|
| AS BUILT REVISIONS DESCRIPTION OF WORK: | N.Y.S. ROUTE 198 (SCAJAQUADA EXPRESSWAY) CORRIDOR I-190 TO N.Y.S. ROUTE 33 CITY OF BUFFALO COUNTY: ERIE | PIN 5470.22 OCTOBER 2016 | BRIDGES | CULVERTS | ALL DIMENSIONS IN m UNLESS OTHERWISE NOTED | CONTRACT NUMBER |  DRAWING NO. SHEET NO. |
| POTENTIAL WATER QUALITY MANAGEMENT AREAS | | | | | | | |
| NEW YORK STATE DEPARTMENT OF TRANSPORTATION REGION 5 | | | | | | | |

EXHIBIT C
EFFLUENT LIMITATION GUIDELINES

FROM GP-0-15-002

Part I.B - Effluent Limitations Applicable to Discharges from Construction Activities

Discharges authorized by this permit must achieve, at a minimum, the effluent limitations in Part I.B.1. (a) – (f) of this permit. These limitations represent the degree of effluent reduction attainable by the application of best practicable technology currently available.

1. Erosion and Sediment Control Requirements – The *owner or operator* must select, design, install, implement and maintain control measures to *minimize the discharge of pollutants* and prevent a violation of the *water quality standards*. The selection, design, installation, implementation, and maintenance of these control measures must meet the non-numeric effluent limitations in Part I.B.1.(a) – (f) of this permit and be in accordance with the New York State Standards and Specifications for Erosion and Sediment Control, dated August 2005, using sound engineering judgement. Where control measures are not designed in conformance with the design criteria included in the technical standard, the *owner or operator* must include in the Stormwater Pollution Prevention Plan (“SWPPP”) the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.
 - a. **Erosion and Sediment Controls.** Design, install and maintain effective erosion and sediment controls to *minimize the discharge of pollutants* and prevent a violation of the *water quality standards*. At a minimum, such controls must be designed, installed and maintained to:
 - i. *Minimize* soil erosion through application of runoff control and soil stabilization control measure to *minimize pollutant discharges*;
 - ii. Control stormwater *discharges* to *minimize* channel and streambank erosion and scour in the immediate vicinity of the *discharge* points;
 - iii. *Minimize* the amount of soil exposed during *construction activity*;
 - iv. *Minimize* the disturbance of *steep slopes*;
 - v. *Minimize* sediment *discharges* from the site;
 - vi. Provide and maintain natural buffers around surface waters, direct stormwater to vegetated areas and maximize stormwater infiltration to reduce *pollutant discharges*, unless *infeasible*;
 - vii. *Minimize* soil compaction. Minimizing soil compaction is not required where the intended function of a specific area of the site dictates that it be compacted; and
 - viii. Unless *infeasible*, preserve a sufficient amount of topsoil to complete soil restoration and establish a uniform, dense vegetative cover.
 - b. **Soil Stabilization.** In areas where soil disturbance activity has temporarily or permanently ceased, the application of soil stabilization measures must be initiated by the end of the next business day and completed within fourteen (14) days from the date the current soil disturbance activity ceased. For construction sites that *directly discharge* to one of the 303(d) segments listing in Appendix E or is location in one of the watersheds listed in Appendix C, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days from the date the current soil disturbance activity ceased. See Appendix A for definition of *Temporarily Ceased*.
 - c. **Dewatering.** *Discharges* from the dewatering activities, including *discharges* from dewatering of trenches and excavations, must be managed by appropriate control measures.

-
- d. **Pollution Prevention Measures.** Design, install, implement, and maintain effective pollution prevention measures to *minimize* the *discharge* of *pollutants* and prevent a violation of the *water quality standards*. At a minimum, such measures must be designed, installed, implemented and maintained to:
- i. *Minimize* the *discharge* of *pollutants* from equipment and vehicle washing, where wash water, and other wash waters. This applies to washing operations that use clean water only. Soaps, detergents and solvents cannot be used.
 - ii. *Minimize* the exposure of building materials, building products, construction wastes, trash, landscape materials, fertilizers, pesticides, herbicides, detergents, sanitary waster and other materials present on the site to precipitation and to stormwater. Minimization of exposure is not required in cases where the exposure to precipitation and to stormwater will not result in a *discharge* of *pollutants*, or where exposure of a specific material or product poses little risk of stormwater contamination (such as final products and materials intended for outdoor use); and
 - iii. Prevent the *discharge* of *pollutants* from spills and leaks and implement chemical spill and leak prevention and response procedures.
- e. **Prohibited Discharges.** The following *discharges* are prohibited:
- i. Wastewater from washout of concrete;
 - ii. Wastewater from washout and cleanout of stucco, paint, form release oils, curing compounds and other construction materials;
 - iii. Fuels, oils, or other *pollutants* used in vehicle and equipment operation and maintenance;
 - iv. Soaps or solvents used in vehicle and equipment washing; and
 - v. Toxic or hazardous substances from a spill or other release.
- f. **Surface Outlets.** When discharging from basins and impoundments, the outlets shall be designed, constructed and maintained in such a manner that sediment does not leave the basin or impoundment and that erosion at or below the outlet does not occur.

EXHIBIT D

WATER QUALITY VOLUME PRELIMINARY SIZING COMPUTATIONS



Project: Scajauada Expressway NYS Route 198

Project No. 6861.00

Date: 10/10/2016

By: KMG

Checked: JAV

Sheet: 1 of 8

Contract 1

~630 ft West of Elmwood to East End of Project

| | |
|---------------------------------|------------------------------|
| Existing Impervious | 110670 sm 27.3 ac |
| Proposed Impervious | 106750 sm 26.4 ac |
| New Impervious | 0 sm 0.0 ac 0% |
| Redev. Impervious | 106750 sm 26.4 ac 100% |
| Removed Impervious | 3920 sm 1.0 ac 4% |
| Est. Disturbed Area | 198875 sm 49.1 ac |
| $I = ((NA+RA)/A)*100 =$ | 54% |
| $Rv = 0.05 + 0.009(I) =$ | 0.533 |
| $WQv_{(initial)} =$ | 2.183 ac-ft 2693 cm |
| % Treatent Req'd | 25% |
| WQv from Pavement Reduction | 95 cm 4% |
| %WQv Req'd by Alt. Practices | 63% |
| WQv Req'd by Alt. Practices | 1.375 ac-ft 1696 cm |
| Practices In Contract 1 | RRv WQv |
| HDS #12 | 2,080 cm |
| Sum | 0 2,080 cm |
| Total WQv Provided - Contract 1 | 2,080 cm |
| Net WQv | -383 cm |

Contract 2

West End of Project to ~630 ft West of Elmwood

| | |
|---------------------------------|----------------------------|
| Existing Impervious | 35355 sm 8.7 ac |
| Proposed Impervious | 31822 sm 7.9 ac |
| New Impervious | 0 sm 0.0 ac 0% |
| Redev. Impervious | 31822 sm 7.9 ac 100% |
| Removed Impervious | 3533 sm 0.9 ac 10% |
| Est. Disturbed Area | 63357 sm 15.7 ac |
| $I = ((NA+RA)/A)*100 =$ | 50% |
| $Rv = 0.05 + 0.009(I) =$ | 0.502 |
| $WQv_{(initial)} =$ | 0.655 ac-ft 808 cm |
| % Treatent Req'd | 25% |
| $WQv_{(target)} =$ | 0.164 ac-ft 202 cm |
| WQv from Pavement Reduction | 20 cm |
| Practices In Contract 2 | RRv WQv |
| Wet Swale #1 | 0 39 cm |
| Bio Area #2 | 122 182 cm |
| Wet Swale #3A | 0 37 cm |
| Wet Swale #3B | 0 22 cm |
| Sum | 122 280 cm |
| Total WQv Provided - Contract 2 | 402 cm |
| Net WQv | -220 cm |



Project: Scajaquada Expressway NYS
Route 198

Project No. 6861.00
Date: 10/10/2016
By: KMG
Checked: JAV
Sheet: 2 of 8

TITLE: **Impervious Areas**

DESCRIPTION: Impervious ares heading east from BIN 1039989 along Scajaquada Expressway NYS Route 198

| <u>Section</u> | <u>New Impervious Area (m²)</u> |
|----------------|--|
| Roadway, Etc. | 122001 |
| Pathways | 16460 |
| | |
| | |

| | |
|-------------------------------|----------------|
| Total (m²) | 138461 |
| Total (sf²) | 1490382 |
| Total (acres) | 34.2 |

Total Impervious Existing = **36.1** Acres

Total Impervious Proposed = **34.2** Acres

Total Impervious Removed = **1.9** Acres

Total New Impervious = **0.0** Acres

Total Redeveloped Impervious = **34.2** Acres

Total Disturbed Area = **65** Acres

53% Impervious



Project:
Scajauada Expressway NYS Route 198

Project No. 6861.00
Date: 10/10/2016
By: KMG
Checked: JAV
Sheet: 3 of 8

TITLE: **WATER QUALITY STORAGE VOLUME**

Water Quality Volume

DESCRIPTION:

Index **1**

STA EB 10+580 to 10+800
Wet Swale #1

Formula for calculating the Water Quality storage volume (WQv) = $\frac{(P)(Rv)(A)}{12}$

| DA (ac) | %IA % | Rv | P (in) | WQv (ac-ft) | WQv (m ³) |
|------------|----------|------|-----------|----------------|--------------------------|
| 3.65 | 80% | 0.77 | 1.00 | 0.23 | 288.6 |

Design Parameters

| | | | | | |
|-----------------|---------------|--------------------|-------------|----------------|---------------|
| Bottom Width, m | <u>0.6</u> | Media Depth, m | <u>0</u> | Check Dams? | <u>Y</u> |
| Side Slopes | <u>2.5</u> | Media Porosity, n | <u>0.25</u> | Dam Height, m | <u>0.3048</u> |
| Slope, m/m | <u>0.0160</u> | Gravel Depth, m | <u>0.0</u> | Dam Spacing, m | <u>19.1</u> |
| Length, m | <u>187</u> | Gravel Porosity, n | <u>0.4</u> | | |
| Manning's n | <u>0.06</u> | | | | |

Water Quality Volume Event

| Q in | CN | Tc hr | la | la/P | qu (cfs/mi ² /in) | Qp cfs | Qp cms |
|---------|----|----------|-------|-------|---------------------------------|-----------|-----------|
| 0.769 | 98 | 0.2 | 0.041 | 0.041 | 1100 | 4.8 | 0.137 |

Assuming No Check Dams

| | |
|---------------------|-------------|
| Velocity, m/s | <u>0.56</u> |
| Normal Depth, m | <u>0.21</u> |
| Detention Time, min | <u>5.5</u> |

Storage Volume

| | | | |
|---------------------------------------|-------------|---|-------------|
| Area behind Check Dam, m ² | <u>0.42</u> | Surface Storage Volume, m ³ | <u>39.1</u> |
| Subsurface Area, m ² | <u>0</u> | Subsurface Storage Volume, m ³ | <u>0</u> |
| Length Provided, m | <u>187</u> | Total Storage Volume, m ³ | <u>39</u> |

Treatment Volumes

| | |
|--------------------------------------|-----------|
| RRv Treatment Percentage, % | <u>0%</u> |
| RRv Treatment Volume, m ³ | <u>0</u> |
| WQv Treatment Volume, m ³ | <u>39</u> |

25-YR Storm Event

| A ac | C | Tc hr | I in/hr | Q ₂₅ cfs | *V ₂₅ ft/s | *Depth ft | Required Swale Depth | |
|---------|------|----------|------------|------------------------|--------------------------|--------------|----------------------|-----|
| | | | | | | | ft | m |
| 3.65 | 0.60 | 0.20 | 4.16 | 9.2 | 2.65 | 0.88 | 1.7 | 0.5 |

*Assumes storage volume behind check dams is completely full prior to event.



Project:
Scajaquada Expressway NYS Route 198

Project No. 6861.00
Date: 10/10/2016
By: KMG
Checked: JAV
Sheet: 4 of 8

TITLE: **WATER QUALITY STORAGE VOLUME**

Index **7**

Water Quality Volume

DESCRIPTION:

Bio Area #2
Gore near W roundabout - completely assumed drainage

Formula for calculating the Water Quality storage volume (WQv) = $\frac{(P)(Rv)(A)}{12}$

P = 90% Rainfall Event = 1.0

I = percent Impervious Cover = 100%

Rv = 0.05 + 0.009(I) = 0.95

A = Acres = 3

Water Quality Storage Volume (acre-feet) = 0.25 **304** Cubic-meters

Preliminary Bioretention Sizing

| | | | | |
|----------------|-------------|--------|---------------|----|
| A _f | 7807 | sf | 725.34 | sm |
| d _f | 2 | ft | | |
| k | 0.5 | ft/day | | |
| h _f | 0.75 | ft | | |
| t _f | 2 | days | | |

- A_f surface area of filter bed (sf)
- d_f filter bed depth (ft)
- k coefficient of permeability of filter media (ft/day)
- h_f average height of water above filter bed (ft)
- t_f design filter bed drain time (days)

Need to store 75% of WQv in prior to filtration

| | |
|--------------|-------------------|
| 228.0 | cm = 75% of WQv |
| 0.23 | m = ponding depth |
| 996.9 | sm = surface area |

Forebay Sizing

| | |
|------------------|----|
| As = 87.0 | sf |
| 8.1 | sm |

| | | |
|-------------|-----------------|------------------------|
| 76.0 | cm = 25% of WQv | |
| 19.5 | =L (m) | 253.3 =Area, sm |
| 13.0 | =W (m) | |
| 0.3 | =D (m) | |

Areas Provided

Forebay Area Provided, cm = **152** ✓

Storage Area Provided, sm = **998** ✓

RRV Treatment Percentage, % **40%**

RRv Treatment Volume Provided, m³ **122**

WQv Treatment Volume Provided, m³ **182**



Project:
Scajauada Expressway NYS Route 198

Project No. 6861.00
Date: 10/10/2016
By: KMG
Checked: JAV
Sheet: 5 of 8

TITLE: **WATER QUALITY STORAGE VOLUME**

Water Quality Volume

DESCRIPTION:

Index **3**

STA EB 11+000 to 11+180
Wet Swale #3A

Formula for calculating the Water Quality storage volume (WQv) = $\frac{(P)(Rv)(A)}{12}$

| DA (ac) | %IA % | Rv | P (in) | WQv (ac-ft) | WQv (m ³) |
|------------|----------|------|-----------|----------------|--------------------------|
| 2.50 | 58% | 0.57 | 1.00 | 0.12 | 146.4 |

Design Parameters

| | | | | | |
|-----------------|--------|--------------------|------|----------------|--------|
| Bottom Width, m | 0.61 | Media Depth, m | 0 | Check Dams? | Y |
| Side Slopes | 2.5 | Media Porosity, n | 0.25 | Dam Height, m | 0.3048 |
| Slope, m/m | 0.0040 | Gravel Depth, m | 0.0 | Dam Spacing, m | 76.2 |
| Length, m | 175 | Gravel Porosity, n | 0.4 | | |
| Manning's n | 0.07 | | | | |

Water Quality Volume Event

| Q in | CN | Tc hr | la | la/P | qu (cfs/mi ² /in) | Qp cfs | Qp cms |
|---------|----|----------|-------|-------|---------------------------------|-----------|-----------|
| 0.569 | 95 | 0.2 | 0.105 | 0.105 | 800 | 1.8 | 0.050 |

Assuming No Check Dams

| | |
|---------------------|------|
| Velocity, m/s | 0.23 |
| Normal Depth, m | 0.20 |
| Detention Time, min | 12.6 |

Storage Volume

| | | | |
|---------------------------------------|------|---|------|
| Area behind Check Dam, m ² | 0.42 | Surface Storage Volume, m ³ | 36.6 |
| Subsurface Area, m ² | 0 | Subsurface Storage Volume, m ³ | 0 |
| Length Provided, m | 175 | Total Storage Volume, m ³ | 37 |

Treatment Volumes

| | |
|--------------------------------------|----|
| RRv Treatment Percentage, % | 0% |
| RRv Treatment Volume, m ³ | 0 |
| WQv Treatment Volume, m ³ | 37 |

25-YR Storm Event

| A ac | C | Tc hr | I in/hr | Q ₂₅ cfs | *V ₂₅ ft/s | *Depth ft | Required Swale Depth | |
|---------|------|----------|------------|------------------------|--------------------------|--------------|----------------------|-----|
| | | | | | | | ft | m |
| 2.50 | 0.60 | 0.20 | 4.16 | 6.3 | 1.12 | 0.91 | 1.7 | 0.5 |

*Assumes storage volume behind check dams is completely full prior to event.



Project:
Scajauada Expressway NYS Route 198

Project No. 6861.00
Date: 10/10/2016
By: KMG
Checked: JAV
Sheet: 6 of 8

TITLE: **WATER QUALITY STORAGE VOLUME**

Water Quality Volume

DESCRIPTION:

Index **4**

STA EB 11+200 to 11+300
Wet Swale #3B

Formula for calculating the Water Quality storage volume (WQv) = $\frac{(P)(Rv)(A)}{12}$

| DA (ac) | %IA % | Rv | P (in) | WQv (ac-ft) | WQv (m ³) |
|------------|----------|------|-----------|----------------|--------------------------|
| 0.85 | 69% | 0.67 | 1.00 | 0.05 | 58.5 |

Design Parameters

| | | | | | |
|-----------------|--------------|--------------------|-------------|----------------|---------------|
| Bottom Width, m | <u>0.61</u> | Media Depth, m | <u>0</u> | Check Dams? | <u>Y</u> |
| Side Slopes | <u>2.5</u> | Media Porosity, n | <u>0.25</u> | Dam Height, m | <u>0.3048</u> |
| Slope, m/m | <u>0.015</u> | Gravel Depth, m | <u>0.0</u> | Dam Spacing, m | <u>20.3</u> |
| Length, m | <u>105</u> | Gravel Porosity, n | <u>0.4</u> | | |
| Manning's n | <u>0.15</u> | | | | |

Water Quality Volume Event

| Q in | CN | Tc hr | la | la/P | qu (cfs/mi ² /in) | Qp cfs | Qp cms |
|---------|----|----------|-------|-------|---------------------------------|-----------|-----------|
| 0.673 | 97 | 0.1 | 0.062 | 0.062 | 900 | 0.8 | 0.023 |

Assuming No Check Dams

| | |
|---------------------|-------------|
| Velocity, m/s | <u>0.11</u> |
| Normal Depth, m | <u>0.07</u> |
| Detention Time, min | <u>15.9</u> |

Storage Volume

| | | | |
|---------------------------------------|-------------|---|-------------|
| Area behind Check Dam, m ² | <u>0.42</u> | Surface Storage Volume, m ³ | <u>21.9</u> |
| Subsurface Area, m ² | <u>0</u> | Subsurface Storage Volume, m ³ | <u>0</u> |
| Length Provided, m | <u>105</u> | Total Storage Volume, m ³ | <u>22</u> |

Treatment Volumes

| | |
|--------------------------------------|-----------|
| RRv Treatment Percentage, % | <u>0%</u> |
| RRv Treatment Volume, m ³ | <u>0</u> |
| WQv Treatment Volume, m ³ | <u>22</u> |

25-YR Storm Event

| A ac | C | Tc hr | I in/hr | Q ₂₅ cfs | *V ₂₅ ft/s | *Depth ft | Required Swale Depth | |
|---------|------|----------|------------|------------------------|--------------------------|--------------|----------------------|-----|
| | | | | | | | ft | m |
| 0.85 | 0.60 | 0.10 | 5.50 | 2.8 | 0.83 | 0.55 | 1.4 | 0.4 |

*Assumes storage volume behind check dams is completely full prior to event.



Project:
Scajaquada Expressway NYS Route 198

Project No. 6861.00
Date: 10/10/2016
By: KMG
Checked: JAV
Sheet: 7 of 8

TITLE: WATER QUALITY STORAGE VOLUME

Water Quality Volume

DESCRIPTION:

Index 15

Hydrodynamic Separators Assumed Vortechs NYSDOT Sizing Criteria
HDS #12

Contract 1A

DA Captured = 12.6 ac

| | |
|----|------|
| I | 100 |
| Rv | 0.95 |
| P | 1 |

WQv 0.9973 ac-ft 43441 cf 1230 cm

**Actual treatment, sizing, and locations to be coordinated with final drainage during final design.

Will be able to capture required drainage area, number/size/location of facilities will vary.

Contract 1B

DA Captured = 8.7 ac

| | |
|----|------|
| I | 100 |
| Rv | 0.95 |
| P | 1 |

WQv 0.6888 ac-ft 30002 cf 850 cm

**Actual treatment, sizing, and locations to be coordinated with final drainage during final design.

Will be able to capture required drainage area, number/size/location of facilities will vary.

EXHIBIT E
TOLER METHOD CALCULATIONS

**NYS Rte 198 Scajaquada Corridor
PIN 5470.14
City of Buffalo, Erie County, NY**

Toler Method - SCAJAQUADA CREEK

$$C = ((T \times M) / (I \times A)) \times K$$

where:

C= Annual Average Concentration of Cl (mg/L)

T= Tons of salt per Lane-mile

M=Number of Lane-miles

I= Inches of Runoff (annual inches of rain {37.6 in} x 0.7)

A=Drainage Area in square miles

K=8.37

Determine No Build Conditions AND Build Alternative Chloride Concentraions (C).

Assumptions

- 1) This analysis uses the overall drainage area to Scajaquada Creek. In addition, the overall upstream watershed area is assumed to have the same land use and roadway characteristics in both existing and proposed conditions. The preferred alternative lane-miles are applied to the Toler Method, but no base T*M value was added for the remainder of the watershed. The values are only good for comparative purposes, not for actual values of concentration at the waterbodies.

NYS Rte 198 Scajaquada Corridor
 PIN 5470.14
 City of Buffalo, Erie County, NY

Toler Analysis - No Build

Project Area
 0.19 sq. miles

Scajaquada Cre
 Total watershed
 26.7

Drainage Area

| | Station | | No. of lanes | Length meters | Total Length meters | Lane Miles miles |
|---|-----------|-----------|--------------|------------------|---------------------------|---------------------|
| | Start | End | | | | |
| State Roads (T= 27 tons/lane-mile) | | | | | | |
| EASTBOUND | | | | | | |
| Route 198-EB | EB 10+478 | EB 12+385 | 2 | 1896 | 3792 | 2.36 |
| Route 198-EB | EB 12+385 | EB 14+000 | 2 | 1603 | 3206 | 1.99 |
| Route 198-EB | EB 14+000 | EB 14+455 | 3 | 254 | 762 | 0.47 |
| Route 198-EB | EB 14+455 | EB 14+532 | 4 | 79 | 316 | 0.20 |
| Route 198-EB | EB 14+532 | EB 14+502 | 3 | 171 | 513 | 0.32 |
| Ramp to Grant Street | EB 10+720 | GSE 1+090 | 2 | 237 | 474 | 0.29 |
| Ramp from Grant Street | GSW 1+802 | EB 11+000 | 1 | 174 | 174 | 0.11 |
| Ramp at Elmwood | E 1+180 | IC 1+000 | 1 | 432 | 432 | 0.27 |
| Off Ramp at Delaware South | EB 12+880 | DS 1+180 | 1 | 268 | 268 | 0.17 |
| On Ramp from Delaware South | EB 12+970 | DS 12+248 | 1 | 254 | 254 | 0.16 |
| Off Ramp at Delaware North | EB 13+150 | DN 1+220 | 1 | 163 | 163 | 0.10 |
| On Ramp from Delaware North | DN 1+060 | EB 13+330 | 1 | 310 | 310 | 0.19 |
| WESTBOUND | | | | | | |
| Route 198-WB | WB 10+478 | WB 12+395 | 2 | 1917 | 3834 | 2.38 |
| Route 198-WB | WB 12+395 | WB 14+000 | 2 | 1660 | 3320 | 2.06 |
| Route 198-WB | WB 14+000 | WB 14+505 | 3 | 445 | 1335 | 0.83 |
| Ramp to Parkside | P 1+030 | WB 14+320 | 1 | 189 | 189 | 0.12 |
| Ramp from Parkside | P 1+040 | WB 14+002 | 1 | 130 | 130 | 0.08 |
| Connector to Nottingham Terrace | WB 13+000 | | 2 | 104 | 208 | 0.13 |
| Nottingham / Elmwood Connector | L 1+050 | E 12+290 | 1 | 510 | 510 | 0.32 |
| Off Ramp to Elmwood | WB 11+920 | EC 1+180 | 1 | 268 | 268 | 0.17 |
| On Ramp from Elmwood | EC 1+160 | WB 11+650 | 1 | 277 | 277 | 0.17 |
| Off Ramp to Grant | WB 11+220 | GN 1+090 | 1 | 248 | 248 | 0.15 |
| On Ramp from Grant | GN 1+090 | WB 10+755 | 1 | 415 | 415 | 0.26 |
| Total | | | | | 21398 | 13.3 |

| | Station | | No. of lanes | Length meters | Total Length Meters | Lane Miles miles |
|---|----------|----------|--------------|------------------|---------------------------|---------------------|
| | Start | End | | | | |
| Local Roads (T= 10 tons/lane-mile) | | | | | | |
| Grant Street | G 1+211 | G 1+375 | 3 | 163 | 489 | 0.30 |
| Grant Street | G 1+375 | G 1+411 | 5 | 38 | 190 | 0.12 |
| Grant Street | G 1+411 | G 1+466 | 4 | 56 | 224 | 0.14 |
| Nottingham Terrace | NT 1+112 | NT 1+000 | 2 | 112 | 224 | 0.14 |
| Delaware South | DS 1+010 | DS 1+060 | 2 | 50 | 100 | 0.06 |
| Delaware South | DS 1+060 | DS 1+180 | 3 | 115 | 345 | 0.21 |
| Delaware South | DS 1+180 | DS 1+250 | 2 | 68 | 136 | 0.08 |
| Delaware South | DS 1+250 | DS 1+138 | 3 | 189 | 567 | 0.35 |
| Delaware North | DN 1+010 | DN 1+220 | 2 | 211 | 422 | 0.26 |
| Delaware North | DN 1+220 | DN 1+444 | 3 | 226 | 678 | 0.42 |
| Agassazi | M 1+007 | M 1+072 | 2 | 56 | 112 | 0.07 |
| Parkside | P 1+000 | P 1+048 | 4 | 41 | 164 | 0.10 |
| Parkside | P 1+048 | P 1+140 | 5 | 92 | 460 | 0.29 |
| Parkside | P 1+140 | P 1+175 | 4 | 34 | 136 | 0.08 |
| Humboldt Pkwy | HP 1+002 | HP 1+137 | 1 | 129 | 129 | 0.08 |
| Lincoln Pkwy Bridge | N 1+006 | N 1+091 | 2 | 85 | 170 | 0.11 |
| Lincoln Pkwy Bridge | N 1+091 | N 1+160 | 1 | 69 | 69 | 0.04 |
| Total | | | | | 4615 | 2.9 |

| | |
|-------------------------------|-----------------|
| Chloride Concentration | 8.1 mg/L |
|-------------------------------|-----------------|

NYS Rte 198 Scajaquada Corridor
 PIN 5470.14
 City of Buffalo, Erie County, NY

Toler Analysis - No Build

Project Area
 0.11 sq. miles

Hoyt Lake
 Total watershed
 25.8

Drainage Area

| | Station | | No. of lanes | Length meters | Total Length meters | Lane Miles miles |
|---|-----------|-----------|--------------|------------------|---------------------------|---------------------|
| | Start | End | | | | |
| State Roads (T= 27 tons/lane-mile) | | | | | | |
| EASTBOUND | | | | | | |
| Route 198-EB | EB 10+478 | EB 12+385 | 2 | | | |
| Route 198-EB | EB 12+385 | EB 14+000 | 2 | 1603 | 3206 | 1.99 |
| Route 198-EB | EB 14+000 | EB 14+455 | 3 | 254 | 762 | 0.47 |
| Route 198-EB | EB 14+455 | EB 14+532 | 4 | 79 | 316 | 0.20 |
| Route 198-EB | EB 14+532 | EB 14+502 | 3 | 172 | 516 | 0.32 |
| Ramp to Grant Street | EB 10+720 | GSE 1+090 | 2 | | | |
| Ramp from Grant Street | GSW 1+802 | EB 11+000 | 1 | | | |
| Ramp at Elmwood | E 1+180 | IC 1+000 | 1 | | | |
| Off Ramp at Delaware South | EB 12+880 | DS 1+180 | 1 | 268 | 268 | 0.17 |
| On Ramp from Delaware South | EB 12+970 | DS 12+248 | 1 | 254 | 254 | 0.16 |
| Off Ramp at Delaware North | EB 13+150 | DN 1+220 | 1 | 163 | 163 | 0.10 |
| On Ramp from Delaware North | DN 1+060 | EB 13+330 | 1 | 310 | 310 | 0.19 |
| WESTBOUND | | | | | | |
| Route 198-WB | WB 10+478 | WB 12+395 | 2 | | | |
| Route 198-WB | WB 12+395 | WB 14+000 | 2 | 1660 | 3320 | 2.06 |
| Route 198-WB | WB 14+000 | WB 14+505 | 3 | 445 | 1335 | 0.83 |
| Ramp to Parkside | P 1+030 | WB 14+320 | 1 | 189 | 189 | 0.12 |
| Ramp from Parkside | P 1+040 | WB 14+002 | 1 | 130 | 130 | 0.08 |
| Connector to Nottingham Terrace | WB 13+000 | | 2 | 104 | 208 | 0.13 |
| Nottingham / Elmwood Connector | L 1+050 | E 12+290 | 1 | | | |
| Off Ramp to Elmwood | WB 11+920 | EC 1+180 | 1 | | | |
| On Ramp from Elmwood | EC 1+160 | WB 11+650 | 1 | | | |
| Off Ramp to Grant | WB 11+220 | GN 1+090 | 1 | | | |
| On Ramp from Grant | GN 1+090 | WB 10+755 | 1 | | | |
| Total | | | | 5631 | 10977 | 6.8 |

| | Station | | No. of lanes | Length meters | Total Length Meters | Lane Miles miles |
|---|----------|----------|--------------|------------------|---------------------------|---------------------|
| | Start | End | | | | |
| Local Roads (T= 10 tons/lane-mile) | | | | | | |
| Grant Street | G 1+211 | G 1+375 | 3 | | | |
| Grant Street | G 1+375 | G 1+411 | 5 | | | |
| Grant Street | G 1+411 | G 1+466 | 4 | | | |
| Nottingham Terrace | NT 1+112 | NT 1+000 | 2 | | | |
| Delaware South | DS 1+010 | DS 1+060 | 2 | 50 | 100 | 0.06 |
| Delaware South | DS 1+060 | DS 1+180 | 3 | 115 | 345 | 0.21 |
| Delaware South | DS 1+180 | DS 1+250 | 2 | 68 | 136 | 0.08 |
| Delaware South | DS 1+250 | DS 1+138 | 3 | 189 | 567 | 0.35 |
| Delaware North | DN 1+010 | DN 1+220 | 2 | 211 | 422 | 0.26 |
| Delaware North | DN 1+220 | DN 1+444 | 3 | 226 | 678 | 0.42 |
| Agassazi | M 1+007 | M 1+072 | 2 | 56 | 112 | 0.07 |
| Parkside | P 1+000 | P 1+048 | 4 | 41 | 164 | 0.10 |
| Parkside | P 1+048 | P 1+140 | 5 | 92 | 460 | 0.29 |
| Parkside | P 1+140 | P 1+175 | 4 | 34 | 136 | 0.08 |
| Humboldt Pkwy | HP 1+002 | HP 1+137 | 1 | 129 | 129 | 0.08 |
| Lincoln Pkwy Bridge | N 1+006 | N 1+091 | 2 | | | |
| Lincoln Pkwy Bridge | N 1+091 | N 1+160 | 1 | | | |
| Total | | | | 1211 | 3249 | 2.0 |

| | |
|-------------------------------|-----------------|
| Chloride Concentration | 4.4 mg/L |
|-------------------------------|-----------------|

NYS Rte 198 Scajaquada Corridor
 PIN 5470.14
 City of Buffalo, Erie County, NY

Toler Analysis - No Build

Project Area
 0.08 sq. miles

Scajaquada Cre
 Total watershed
 26.7

Drainage Area

| | Station | | No. of lanes | Length meters | Total Length meters | Lane Miles miles |
|---|-----------|-----------|--------------|------------------|---------------------------|---------------------|
| | Start | End | | | | |
| State Roads (T= 27 tons/lane-mile) | | | | | | |
| EASTBOUND | | | | | | |
| Route 198-EB | EB 10+478 | EB 12+385 | 2 | 1896 | 3792 | 2.36 |
| Route 198-EB | EB 12+385 | EB 14+000 | 2 | 1603 | | |
| Route 198-EB | EB 14+000 | EB 14+455 | 3 | 254 | | |
| Route 198-EB | EB 14+455 | EB 14+532 | 4 | 79 | | |
| Route 198-EB | EB 14+532 | EB 14+502 | 3 | 171 | | |
| Ramp to Grant Street | EB 10+720 | GSE 1+090 | 2 | 237 | 474 | 0.29 |
| Ramp from Grant Street | GSW 1+802 | EB 11+000 | 1 | 174 | 174 | 0.11 |
| Ramp at Elmwood | E 1+180 | IC 1+000 | 1 | 432 | 432 | 0.27 |
| Off Ramp at Delaware South | EB 12+880 | DS 1+180 | 1 | 268 | | |
| On Ramp from Delaware South | EB 12+970 | DS 12+248 | 1 | 254 | | |
| Off Ramp at Delaware North | EB 13+150 | DN 1+220 | 1 | 163 | | |
| On Ramp from Delaware North | DN 1+060 | EB 13+330 | 1 | 310 | | |
| WESTBOUND | | | | | | |
| Route 198-WB | WB 10+478 | WB 12+395 | 2 | 1917 | 3834 | 2.38 |
| Route 198-WB | WB 12+395 | WB 14+000 | 2 | 1660 | | |
| Route 198-WB | WB 14+000 | WB 14+505 | 3 | 445 | | |
| Ramp to Parkside | P 1+030 | WB 14+320 | 1 | 189 | | |
| Ramp from Parkside | P 1+040 | WB 14+002 | 1 | 130 | | |
| Connector to Nottingham Terrace | WB 13+000 | | 2 | 104 | | |
| Nottingham / Elmwood Connector | L 1+050 | E 12+290 | 1 | 510 | 510 | 0.32 |
| Off Ramp to Elmwood | WB 11+920 | EC 1+180 | 1 | 268 | 268 | 0.17 |
| On Ramp from Elmwood | EC 1+160 | WB 11+650 | 1 | 277 | 277 | 0.17 |
| Off Ramp to Grant | WB 11+220 | GN 1+090 | 1 | 248 | 248 | 0.15 |
| On Ramp from Grant | GN 1+090 | WB 10+755 | 1 | 415 | 415 | 0.26 |
| Total | | | | | 10424 | 6.5 |

| | Station | | No. of lanes | Length meters | Total Length Meters | Lane Miles miles |
|---|----------|----------|--------------|------------------|---------------------------|---------------------|
| | Start | End | | | | |
| Local Roads (T= 10 tons/lane-mile) | | | | | | |
| Grant Street | G 1+211 | G 1+375 | 3 | 163 | 489 | 0.30 |
| Grant Street | G 1+375 | G 1+411 | 5 | 38 | 190 | 0.12 |
| Grant Street | G 1+411 | G 1+466 | 4 | 56 | 224 | 0.14 |
| Nottingham Terrace | NT 1+112 | NT 1+000 | 2 | 112 | 224 | 0.14 |
| Delaware South | DS 1+010 | DS 1+060 | 2 | 50 | | |
| Delaware South | DS 1+060 | DS 1+180 | 3 | 115 | | |
| Delaware South | DS 1+180 | DS 1+250 | 2 | 68 | | |
| Delaware South | DS 1+250 | DS 1+138 | 3 | 189 | | |
| Delaware North | DN 1+010 | DN 1+220 | 2 | 211 | | |
| Delaware North | DN 1+220 | DN 1+444 | 3 | 226 | | |
| Agassazi | M 1+007 | M 1+072 | 2 | 56 | | |
| Parkside | P 1+000 | P 1+048 | 4 | 41 | | |
| Parkside | P 1+048 | P 1+140 | 5 | 92 | | |
| Parkside | P 1+140 | P 1+175 | 4 | 34 | | |
| Humboldt Pkwy | HP 1+002 | HP 1+137 | 1 | 129 | | |
| Lincoln Pkwy Bridge | N 1+006 | N 1+091 | 2 | 85 | 170 | 0.11 |
| Lincoln Pkwy Bridge | N 1+091 | N 1+160 | 1 | 69 | 69 | 0.04 |
| Total | | | | | 1366 | 0.8 |

| | |
|-------------------------------|-----------------|
| Chloride Concentration | 3.8 mg/L |
|-------------------------------|-----------------|

Toler Analysis - Build Alternative

Drainage Area

Project Area
 0.19 sq. miles

Scajauada Creek
 Total watershed
 26.7 sq. miles

| | From STA | To STA | No. of lanes | Length | Total | Lane Miles |
|---|-----------|-----------|--------------|--------------------|------------------|-------------------|
| | | | | meters Proposed | Length Meters | miles Proposed |
| 198 Roadways (T = 27 tons/lane-mile) | | | | | | |
| EB 198 | EB 10+478 | EB 10+773 | 2 | 293 | 586 | 0.36 |
| EB 198 TO ROUNDABOUT | EB 10+773 | GSE 1+000 | 3 | 95 | 285 | 0.18 |
| Roundabout | GR 1+000 | GR 1+040 | 1 | 150 | 150 | 0.09 |
| EB 198 | EB 10+900 | EB 12+385 | 2 | 1485 | 2970 | 1.85 |
| EB 198 | EB 12+385 | EB 13+120 | 2 | 738 | 1476 | 0.92 |
| EB 198 | EB 13+120 | EB 13+212 | 3 | 89 | 267 | 0.17 |
| EB 198 | EB 13+212 | EB 13+910 | 2 | 692 | 1384 | 0.86 |
| EB 198 | EB 13+910 | EB 13+975 | 3 | 67 | 201 | 0.12 |
| EB 198 | EB 13+975 | EB 14+130 | 4 | 155 | 620 | 0.39 |
| EB 198 | EB 14+130 | EB 14+200 | 3 | 72 | 216 | 0.13 |
| EB 198 | EB 14+200 | EB 14+340 | 4 | 136 | 544 | 0.34 |
| EB 198 | EB 14+340 | EB 14+505 | 3 | 167 | 501 | 0.31 |
| WB 198 | WB 10+478 | WB 11+785 | 2 | 1311 | 2622 | 1.63 |
| WB 198 | WB 11+785 | WB 11+910 | 3 | 122 | 366 | 0.23 |
| WB 198 | WB 11+910 | WB 12+395 | 2 | 486 | 972 | 0.60 |
| WB 198 | WB 12+395 | WB 13+240 | 2 | 844 | 1688 | 1.05 |
| WB 198 | WB 13+240 | WB 13+400 | 4 | 160 | 640 | 0.40 |
| WB 198 | WB 13+400 | WB 13+790 | 2 | 388 | 776 | 0.48 |
| WB 198 | WB 13+790 | WB 13+860 | 3 | 72 | 216 | 0.13 |
| WB 198 | WB 13+860 | WB 13+935 | 2 | 76 | 152 | 0.09 |
| WB 198 | WB 13+935 | WB 14+140 | 3 | 202 | 606 | 0.38 |
| WB 198 | WB 14+140 | WB 14+270 | 5 | 129 | 645 | 0.40 |
| WB 198 | WB 14+270 | WB 14+320 | 4 | 54 | 216 | 0.13 |
| WB 198 | WB 14+320 | WB 14+508 | 3 | 184 | 552 | 0.34 |
| Grant Street East Connector | GSE 1+00 | GSE 1+074 | 3 | 75 | 225 | 0.14 |
| Grant Street West Connector | GSW 1+00 | GSW 1+065 | 2 | 62 | 124 | 0.08 |
| Ramp DC | DC 1+000 | DC 1+160 | 5 | 158 | 790 | 0.49 |
| Ramp L | L 1+010 | L 1+070 | 1 | 61 | 61 | 0.04 |
| Grant Street North Connector | GN 1+220 | GN 1+135 | 2 | 84 | 168 | 0.10 |
| Grant Street North Connector | GN 1+135 | GN 1+070 | 3 | 66 | 198 | 0.12 |
| Parkside Ramp | P 1+040 | WB 14+100 | 1 | 35 | 35 | 0.02 |
| Total | | | | | 20252 | 12.6 |

| | From STA | To STA | No. of lanes | Length | Total | Lane Miles |
|--|----------|----------|--------------|--------------------|------------------|-------------------|
| | | | | meters Proposed | Length Meters | miles Proposed |
| Local Roads (T = 10 tons/lane-mile) | | | | | | |
| Agassai | M 1+008 | M 1+063 | 3 | 55 | 165 | 0.10 |
| Parkside | P 1+008 | P 1+100 | 4 | 59 | 236 | 0.15 |
| Parkside | P 1+100 | P 1+170 | 3 | 73 | 219 | 0.14 |
| Humboldt Pkwy | HP 1+138 | HP 1+010 | 1 | 130 | 130 | 0.08 |
| Ramp from Parkside | P 1+140 | P 1+040 | 1 | 98 | 98 | 0.06 |
| Delaware North | DN 1+010 | DN 1+095 | 2 | 85 | 170 | 0.11 |
| Delaware North | DN 1+095 | DN 1+175 | 3 | 84 | 252 | 0.16 |
| Delaware North | DN 1+175 | DN 1+395 | 2 | 217 | 434 | 0.27 |
| Delaware North | DN 1+395 | DN 1+442 | 3 | 50 | 150 | 0.09 |
| Delaware South | DS 1+438 | DS 1+345 | 2 | 88 | 176 | 0.11 |
| Delaware South | DS 1+442 | DS 1+295 | 3 | 52 | 156 | 0.10 |
| Delaware South | DS 1+295 | DS 1+170 | 4 | 130 | 520 | 0.32 |
| Delaware South | DS 1+170 | DS 1+010 | 2 | 154 | 308 | 0.19 |
| Nottingham Terrace | NT 1+010 | NT 1+112 | 3 | 112 | 336 | 0.21 |
| Grant Street | G 1+210 | G 1+270 | 3 | 56 | 168 | 0.10 |
| Grant Street | G 1+270 | G 1+350 | 4 | 105 | 420 | 0.26 |
| Grant Street | G 1+350 | G 1+425 | 5 | 53 | 265 | 0.16 |
| Grant Street | G 1+425 | G 1+465 | 4 | 43 | 172 | 0.11 |
| New Elmwood Connector Street | EC 1+005 | EC 1+060 | 4 | 55 | 220 | 0.14 |
| New Elmwood Connector Street | EC 1+060 | EC 1+180 | 5 | 121 | 605 | 0.38 |
| Lincoln Pkwy Bridge | N 1+006 | N 1+160 | 1 | 155 | 155 | 0.10 |
| Total | | | | | 5,355 | 3.3 |

** Previously as state

| | |
|-------------------------------|-----------------|
| Chloride Concentration | 7.8 mg/L |
|-------------------------------|-----------------|

Toler Analysis - Build Alternative

Project Area
 0.11 sq. miles

Hoyt Lake
 Total watershed
 25.8 sq. miles

Drainage Area

| | From STA | To STA | No. of lanes | Length | Total | Lane Miles |
|---|-----------|-----------|--------------|--------------------|------------------|-------------------|
| | | | | meters Proposed | Length Meters | miles Proposed |
| 198 Roadways (T = 27 tons/lane-mile) | | | | | | |
| EB 198 | EB 10+478 | EB 10+773 | 2 | | | |
| EB 198 TO ROUNDABOUT | EB 10+773 | GSE 1+000 | 3 | | | |
| Roundabout | GR 1+000 | GR 1+040 | 1 | | | |
| EB 198 | EB 10+900 | EB 12+385 | 2 | | | |
| EB 198 | EB 11+640 | EB 11+770 | 2 | | | |
| EB 198 | EB 12+385 | EB 13+120 | 2 | 737 | 1474 | 0.92 |
| EB 198 | EB 13+120 | EB 13+212 | 3 | 88 | 264 | 0.16 |
| EB 198 | EB 13+212 | EB 13+910 | 2 | 691 | 1382 | 0.86 |
| EB 198 | EB 13+910 | EB 13+975 | 3 | 66 | 198 | 0.12 |
| EB 198 | EB 13+975 | EB 14+130 | 4 | 154 | 616 | 0.38 |
| EB 198 | EB 14+130 | EB 14+200 | 3 | 71 | 213 | 0.13 |
| EB 198 | EB 14+200 | EB 14+340 | 4 | 135 | 540 | 0.34 |
| EB 198 | EB 14+340 | EB 14+505 | 3 | 166 | 498 | 0.31 |
| WB 198 | WB 10+478 | WB 11+785 | 2 | | | |
| WB 198 | WB 11+785 | WB 11+910 | 3 | | | |
| WB 198 | WB 11+910 | WB 12+395 | 2 | | | |
| WB 198 | WB 12+395 | WB 13+240 | 2 | 843 | 1686 | 1.05 |
| WB 198 | WB 13+240 | WB 13+400 | 4 | 160 | 640 | 0.40 |
| WB 198 | WB 13+400 | WB 13+790 | 2 | 387 | 774 | 0.48 |
| WB 198 | WB 13+790 | WB 13+860 | 3 | 72 | 216 | 0.13 |
| WB 198 | WB 13+860 | WB 13+935 | 2 | 76 | 152 | 0.09 |
| WB 198 | WB 13+935 | WB 14+140 | 3 | 201 | 603 | 0.37 |
| WB 198 | WB 14+140 | WB 14+270 | 5 | 128 | 640 | 0.40 |
| WB 198 | WB 14+270 | WB 14+320 | 4 | 54 | 216 | 0.13 |
| WB 198 | WB 14+320 | WB 14+508 | 3 | 184 | 552 | 0.34 |
| Grant Street East Connector | GSE 1+00 | GSE 1+074 | 3 | | | |
| Grant Street West Connector | GSW 1+00 | GSW 1+065 | 2 | | | |
| Ramp DC | DC 1+000 | DC 1+160 | 5 | 158 | 790 | 0.49 |
| Ramp L | L 1+010 | L 1+070 | 1 | 61 | 61 | 0.04 |
| Grant Street North Connector | GN 1+220 | GN 1+135 | 2 | | | |
| Grant Street North Connector | GN 1+135 | GN 1+070 | 3 | | | |
| Parkside Ramp | P 1+040 | WB 14+100 | 1 | 35 | 35 | 0.02 |
| Total | | | | 4467 | 11550 | 7.2 |

| | From STA | To STA | No. of lanes | Length | Total | Lane Miles |
|--|----------|----------|--------------|--------------------|------------------|-------------------|
| | | | | meters Proposed | Length Meters | miles Proposed |
| Local Roads (T = 10 tons/lane-mile) | | | | | | |
| Agassai | M 1+008 | M 1+063 | 3 | 56 | 168 | 0.10 |
| Parkside | P 1+008 | P 1+100 | 4 | 59 | 236 | 0.15 |
| Parkside | P 1+100 | P 1+170 | 3 | 73 | 219 | 0.14 |
| Humboldt Pkwy | HP 1+138 | HP 1+010 | 1 | 129 | 129 | 0.08 |
| Ramp from Parkside | P 1+140 | P 1+040 | 1 | 98 | 98 | 0.06 |
| Delaware North | DN 1+010 | DN 1+095 | 2 | 85 | 170 | 0.11 |
| Delaware North | DN 1+095 | DN 1+175 | 3 | 84 | 252 | 0.16 |
| Delaware North | DN 1+175 | DN 1+395 | 2 | 217 | 434 | 0.27 |
| Delaware North | DN 1+395 | DN 1+442 | 3 | 50 | 150 | 0.09 |
| Delaware South | DS 1+438 | DS 1+345 | 2 | 88 | 176 | 0.11 |
| Delaware South | DS 1+442 | DS 1+295 | 3 | 52 | 156 | 0.10 |
| Delaware South | DS 1+295 | DS 1+170 | 4 | 130 | 520 | 0.32 |
| Delaware South | DS 1+170 | DS 1+010 | 2 | 153 | 306 | 0.19 |
| Nottingham Terrace | NT 1+010 | NT 1+112 | 3 | | | |
| Grant Street | G 1+210 | G 1+270 | 3 | | | |
| Grant Street | G 1+270 | G 1+350 | 4 | | | |
| Grant Street | G 1+350 | G 1+425 | 5 | | | |
| Grant Street | G 1+425 | G 1+465 | 4 | | | |
| New Elmwood Connector Street | EC 1+005 | EC 1+060 | 4 | | | |
| New Elmwood Connector Street | EC 1+060 | EC 1+180 | 5 | | | |
| Lincoln Pkwy Bridge | N 1+006 | N 1+160 | 1 | | | |
| Total | | | | 1274 | 3,014 | 1.9 |

** Previously as state

| | |
|-------------------------------|-----------------|
| Chloride Concentration | 4.6 mg/L |
|-------------------------------|-----------------|

Toler Analysis - Build Alternative

Drainage Area

Project Area
 0.08 sq. miles

Scajaquada Creek
 Total watershed
 26.7 sq. miles

| | From STA | To STA | No. of lanes | Length | Total | Lane Miles |
|---|-----------|-----------|--------------|----------|-------------|------------|
| | | | | meters | Length | miles |
| | | | | Proposed | Meters | Proposed |
| 198 Roadways (T = 27 tons/lane-mile) | | | | | | |
| EB 198 | EB 10+478 | EB 10+773 | 2 | 293 | 586 | 0.36 |
| EB 198 TO ROUNDABOUT | EB 10+773 | GSE 1+000 | 3 | 95 | 285 | 0.18 |
| Roundabout | GR 1+000 | GR 1+040 | 1 | 150 | 150 | 0.09 |
| EB 198 | EB 10+900 | EB 12+385 | 2 | 1485 | 2970 | 1.85 |
| EB 198 | EB 11+640 | EB 11+770 | 2 | 130 | 260 | 0.16 |
| EB 198 | EB 12+385 | EB 13+120 | 2 | 738 | | |
| EB 198 | EB 13+120 | EB 13+212 | 3 | 89 | | |
| EB 198 | EB 13+212 | EB 13+910 | 2 | 692 | | |
| EB 198 | EB 13+910 | EB 13+975 | 3 | 67 | | |
| EB 198 | EB 13+975 | EB 14+130 | 4 | 155 | | |
| EB 198 | EB 14+130 | EB 14+200 | 3 | 72 | | |
| EB 198 | EB 14+200 | EB 14+340 | 4 | 136 | | |
| EB 198 | EB 14+340 | EB 14+505 | 3 | 167 | | |
| WB 198 | WB 10+478 | WB 11+785 | 2 | 1311 | 2622 | 1.63 |
| WB 198 | WB 11+785 | WB 11+910 | 3 | 122 | 366 | 0.23 |
| WB 198 | WB 11+910 | WB 12+395 | 2 | 486 | 972 | 0.60 |
| WB 198 | WB 12+395 | WB 13+240 | 2 | 844 | | |
| WB 198 | WB 13+240 | WB 13+400 | 4 | 160 | | |
| WB 198 | WB 13+400 | WB 13+790 | 2 | 388 | | |
| WB 198 | WB 13+790 | WB 13+860 | 3 | 72 | | |
| WB 198 | WB 13+860 | WB 13+935 | 2 | 76 | | |
| WB 198 | WB 13+935 | WB 14+140 | 3 | 202 | | |
| WB 198 | WB 14+140 | WB 14+270 | 5 | 129 | | |
| WB 198 | WB 14+270 | WB 14+320 | 4 | 54 | | |
| WB 198 | WB 14+320 | WB 14+508 | 3 | 184 | | |
| Grant Street East Connector | GSE 1+00 | GSE 1+074 | 3 | 75 | 225 | 0.14 |
| Grant Street West Connector | GSW 1+00 | GSW 1+065 | 2 | 62 | 124 | 0.08 |
| Ramp DC | DC 1+000 | DC 1+160 | 5 | 158 | | |
| Ramp L | L 1+010 | L 1+070 | 1 | 61 | | |
| Grant Street North Connector | GN 1+220 | GN 1+135 | 2 | 84 | 168 | 0.10 |
| Grant Street North Connector | GN 1+135 | GN 1+070 | 3 | 66 | 198 | 0.12 |
| Parkside Ramp | P 1+040 | WB 14+100 | 1 | 35 | | |
| | | | | | | |
| | | | | | | |
| Total | | | | | 8926 | 5.5 |

| | From STA | To STA | No. of lanes | Length | Total | Lane Miles |
|--|-----------|-----------|--------------|----------|--------------|------------|
| | | | | meters | Length | miles |
| | | | | Proposed | Meters | Proposed |
| Local Roads (T = 10 tons/lane-mile) | | | | | | |
| Agassai | M 1+008 | M 1+063 | 3 | 55 | | |
| Parkside | P 1+008 | P 1+100 | 4 | 59 | | |
| Parkside | P 1+100 | P 1+170 | 3 | 73 | | |
| Humboldt Pkwy | HP 1+138 | HP 1+010 | 1 | 130 | | |
| Ramp from Parkside | P 1+140 | P 1+040 | 1 | 98 | | |
| Ramp to Parking Area | DPA 1+012 | DPA 1+100 | 1 | 83 | | |
| Delaware North | DN 1+010 | DN 1+095 | 2 | 85 | | |
| Delaware North | DN 1+095 | DN 1+175 | 3 | 84 | | |
| Delaware North | DN 1+175 | DN 1+395 | 2 | 217 | | |
| Delaware North | DN 1+395 | DN 1+442 | 3 | 50 | | |
| Delaware South | DS 1+438 | DS 1+345 | 2 | 88 | | |
| Delaware South | DS 1+442 | DS 1+295 | 3 | 52 | | |
| Delaware South | DS 1+295 | DS 1+170 | 4 | 130 | | |
| Delaware South | DS 1+170 | DS 1+010 | 2 | 154 | | |
| Nottingham Terrace | NT 1+010 | NT 1+112 | 3 | 112 | 336 | 0.21 |
| Grant Street | G 1+210 | G 1+270 | 3 | 56 | 168 | 0.10 |
| Grant Street | G 1+270 | G 1+350 | 4 | 105 | 420 | 0.26 |
| Grant Street | G 1+350 | G 1+425 | 5 | 53 | 265 | 0.16 |
| Grant Street | G 1+425 | G 1+465 | 4 | 43 | 172 | 0.11 |
| New Elmwood Connector Street | EC 1+005 | EC 1+060 | 4 | 55 | 220 | 0.14 |
| New Elmwood Connector Street | EC 1+060 | EC 1+180 | 5 | 121 | 605 | 0.38 |
| Lincoln Pkwy Bridge | N 1+006 | N 1+160 | 1 | 154 | 154 | 0.10 |
| | | | | | | |
| Total | | | | | 2,340 | 1.5 |

** Previously as state

| | |
|-------------------------------|-----------------|
| Chloride Concentration | 3.4 mg/L |
|-------------------------------|-----------------|

EXHIBIT F
POLLUTANT LOADING CALCULATIONS

The Simple Method- from the NYS Stormwater Design Manual (2001)

$$L = 0.226 * R * C * A$$

where:
L= Annual Load in lbs.
R= Annual Runoff in inches*
C= Pollutant Concentration (mg/L)
A= Area (acres)
0.226= unit conversion factor

where:
Runoff: $R = R_v * P * P_j$
R= Annual Runoff (inches)
P= Annual Rainfall (inches)
P_j = Fraction of events that produce runoff, usually 0.9
R_v= Runoff Coefficient

$$\text{and } R_v = (0.05) + (0.009 * I_a)$$

where: I_a=Impervious Fraction**

* Annual rainfall was taken from USGS Stream Stats = 37.6"

** Areas include only the existing and proposed impervious areas (not including pathways) giving you a total of 100% impervious area.

Pollutant Concentrations from Urban Highway

| Pollutant | Units | Concentration |
|-----------|-------|---------------|
| TSS | mg/L | 142.00 |
| TP | mg/L | 0.32 |
| TN | mg/L | 3.00 |
| Cu | mg/L | 0.05 |
| Pb | mg/L | 0.40 |
| Zn | mg/L | 0.33 |

* Concentrations taken from p. A-3 from the NYS Stormwater Management Design Manual (2001)

No Build Alternative

a. Area acres

b. Percent Impervious, Ia

c. Runoff Coefficient, Rv dimensionless

d. Runoff, R inches

e. Annual load

| | | | | |
|-----|-------------------------------------|------|-------------------------------------|-----|
| TSS | <input type="text" value="37,244"/> | lbs. | <input type="text" value="16,894"/> | kgs |
| TP | <input type="text" value="84"/> | lbs. | <input type="text" value="38"/> | kgs |
| TN | <input type="text" value="787"/> | lbs. | <input type="text" value="357"/> | kgs |
| Cu | <input type="text" value="14"/> | lbs. | <input type="text" value="6"/> | kgs |
| Pb | <input type="text" value="105"/> | lbs. | <input type="text" value="48"/> | kgs |
| Zn | <input type="text" value="86"/> | lbs. | <input type="text" value="39"/> | kgs |

Pollutant Concentrations from Urban Highway

| Pollutant | Units | Concentration |
|-----------|-------|---------------|
| TSS | mg/L | 142.00 |
| TP | mg/L | 0.32 |
| TN | mg/L | 3.00 |
| Cu | mg/L | 0.05 |
| Pb | mg/L | 0.40 |
| Zn | mg/L | 0.33 |

* Concentrations taken from p. A-3 from the NYS Stormwater Management Design Manual

Build Alternative

a. Area acres (does not include walkways)

b. Percent Impervious, Ia ratio

c. Runoff Coefficient, Rv dimensionless

d. Runoff, R inches

e. Annual load

| | | |
|-----|--|---|
| TSS | <input type="text" value="31,106"/> lbs. | <input type="text" value="14,109"/> kgs |
| TP | <input type="text" value="70"/> lbs. | <input type="text" value="32"/> kgs |
| TN | <input type="text" value="657"/> lbs. | <input type="text" value="298"/> kgs |
| Cu | <input type="text" value="12"/> lbs. | <input type="text" value="5"/> kgs |
| Pb | <input type="text" value="88"/> lbs. | <input type="text" value="40"/> kgs |
| Zn | <input type="text" value="72"/> lbs. | <input type="text" value="33"/> kgs |

Anticipated Pollutant Removal Based on Stormwater Management

| Facility | IA Treated (ac) | % of Total DA | TSS | | TP | | TN | | Cu | | Pb | | Zn | |
|-------------------------------------|-----------------|---------------|----------------|---------------|----------------|---------------|----------------|---------------|----------------|---------------|----------------|---------------|----------------|---------------|
| | | | Efficiency (%) | Removed (lbs) |
| Swale #1 | 2.9 | 10% | 81% | 2440 | 24% | 1.6 | 56% | 36 | 65% | 0.7 | | 0 | 71% | 5.0 |
| Bio Area #2 | 3.1 | 10% | 59% | 1893 | 5% | 0.4 | 46% | 31 | 81% | 1.0 | | 0 | 79% | 5.9 |
| Swale #3A | 1.5 | 5% | 81% | 1212 | 24% | 0.8 | 56% | 18 | 65% | 0.4 | | 0 | 71% | 2.5 |
| Swale #3B | 0.6 | 2% | 81% | 490 | 24% | 0.3 | 56% | 7 | 65% | 0.1 | | 0 | 71% | 1.0 |
| Hydrodynamic | 21.3 | 71% | 55% | 12086 | 81% | 40.1 | 10% | 46 | | 0.0 | | 0 | | 0.0 |
| Total Removed from SWM | 29.4 | 97% | | 18121 | | 43 | | 138 | | 2.3 | | 0 | | 14 |
| Total Removed from Pavement Removal | | | | 6139 | | 14 | | 130 | | 2.3 | | 17 | | 14 |
| Total Removed | | | | 24260 | | 57 | | 268 | | 4.6 | | 17 | | 29 |
| Total Reduction % | | | | 65% | | 68% | | 34% | | 32% | | 16% | | 33% |

**Removal efficiencies from various sources including:

National Pollutant Removal Performance Database, Version 3. September 2007. Center for Watershed Protection.

NYS Stormwater Design Manual. January 2015. New York State Department of Environmental Conservation.

New Hampshire Stormwater Manual, Volume 2. December 2008. New Hampshire Department of Environmental Services.

Some pollutant removal efficiency values for various treatment practices were unable to be found in cited literature.